

On the influence of surface quenching, electron emission and surface recombination on discharge properties

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73rd Gaseous Electronics Conference, Virtual Conference,
October 5, 2020



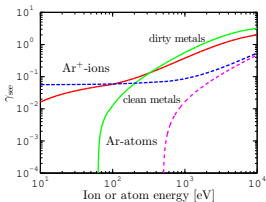
Introduction

- The various plasma surface interaction processes have a significant influence on discharge properties
- In discharge modeling these processes are commonly described by parameters that give the probability of occurrence of the process such as
 - surface recombination to form molecules
 - surface quenching of metastable states
 - electron emission from surfaces due to ion, electron and neutral bombardment of surfaces
 - species reflection from surfaces
 - sputter yields due to ion bombardment
 - surface sticking probabilities for atoms and molecules
- The surface interaction parameters, often describe a complex processes, that are not well understood, by a single number

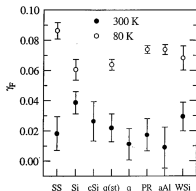


Introduction

- These parameters depend on surface temperature, surface type as well as the discharge properties
- Emission of secondary electrons can result from bombardment of electrons, ions or neutrals on a surface
- The yield γ_{see} is defined as the number of secondary electrons emitted per incident species
- The surface recombination probability γ_F of fluorine atoms on various surfaces at 300 and 80 K



PHELPS ET AL. PSST 8 R21 AND PSST 8 B1



Outline

- 1. Atom surface recombination
 - 1.1. Inductively coupled oxygen discharge
 - 1.2. Inductively coupled chlorine discharge
- 2. Surface quenching of metastable molecules
 - Capacitively coupled oxygen discharge
- 3. Sputter yield
 - Reactive high power impulse magnetron sputtering (HiPIMS)

1. Atom surface recombination

A global (volume averaged) model study



The global (volume averaged) model

- The wall recombination coefficient γ_{rec} is one of the most important parameters in molecular discharge modelling
- In the global model the diffusional losses of neutral atoms to the reactor walls are given by

$$k_{\text{atom,wall}} = \left[\frac{\Lambda_{\text{atom}}^2}{D_{\text{atom}}} + \frac{2V(2 - \gamma_{\text{rec}})}{Av_{\text{atom}}\gamma_{\text{rec}}} \right]^{-1} \text{ s}^{-1}$$

- D_{atom} is the diffusion coefficient for neutral atoms
- $v_{\text{atom}} = (8eT_g/\pi m_{\text{atom}})^{1/2}$ is the mean atom velocity
- γ_{rec} is the wall recombination coefficient for neutral atoms on the wall surface
- Λ_{atom} is the effective diffusion length of neutral atoms

$$\Lambda_{\text{atom}} = \left[\left(\frac{\pi}{L} \right)^2 + \left(\frac{2.405}{R} \right)^2 \right]^{-1/2}$$



1.1. Inductively coupled Oxygen discharge



Surface recombination

- The pressure dependence on the wall recombination coefficient was achieved by fitting all the available data for stainless steel surfaces
- For anodized aluminium reactor walls the recombination coefficient is assumed to be a constant $\gamma_{\text{rec}} = 0.06$ (Guha et al., 2008)
- The same wall recombination coefficient was used for O(¹D) as no data is available

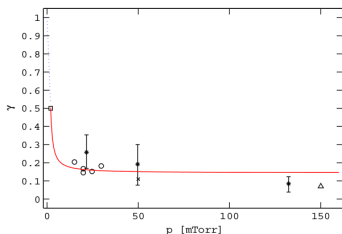


Figure 1. The recombination coefficient of oxygen atoms at the chamber walls for stainless steel as a function of pressure. The measured data is taken from, o Singh *et al* [47], x Matsushita *et al* [90], Δ Mozetič and Zalar [91], \square Booth and Sadeghi [44] and * Gomez *et al* [46]. The solid line shows a fit to the measured data and the dotted line is a linear extrapolation from $\gamma = 0.5$ at 2 mTorr to $\gamma = 1.0$ at vacuum.

The wall recombination coefficient for oxygen atoms on stainless steel surfaces depends on pressure through

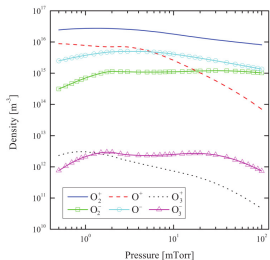
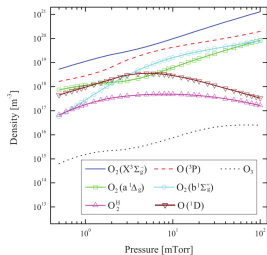
$$\gamma_{\text{rec}} = 0.1438 \exp(2.5069/p) \quad p > 2 \text{ mTorr}$$

$$\gamma_{\text{rec}} = -0.25p + 1 \quad p < 2 \text{ mTorr}$$

Particle densities

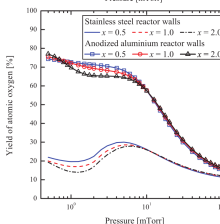
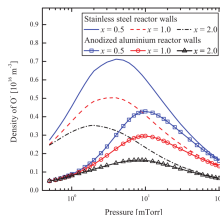
- The dominant species is the oxygen molecule in the ground state $O_2(X^3\Sigma_g)$ followed by the oxygen atom in the ground state $O(^3P)$
- The singlet metastable states $O_2(a^1\Delta_g)$ and $O_2(b^1\Sigma_g^+)$ and the metastable atom $O(^1D)$ are also present in the plasma in significant amounts
- a cylindrical stainless steel chamber
radius $R = 15$ cm and length $L = 30$ cm $P_{abs} = 500$ W

Toneli et al. (2015a) J. Phys. D **48** 325202



Influence of chamber wall and EEDF

- The chamber wall has a significant influence on the dissociation fraction
 - the dissociation fraction is much higher for anodized aluminium reactor walls
- The parameter x defines the shape of the electron energy distribution
 - $x = 0.5$ is concave or bi-Maxwellian
 - $x = 1$ is Maxwellian distribution
 - $x = 2$ is Druyvesteyn distribution

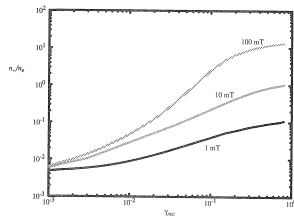
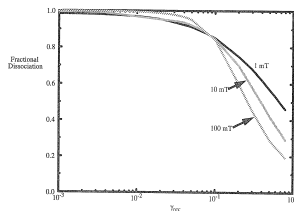


1.2. Inductively coupled Chlorine discharge



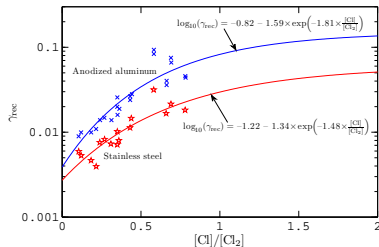
Surface recombination

- Chlorine is widely used in plasma etching of both semiconductors and metals and chlorine atoms are believed to be the primary reactant
- The dissociation fraction and electronegativity versus the surface recombination of atomic chlorine
- For a large γ_{rec} , the fractional dissociation decreases
- For the $\gamma_{\text{rec}} = 0.1$ the chlorine discharge is 80 % dissociated
- The negative ion density exceeds the electron density at $\gamma_{\text{rec}} = 0.08$ at a pressure of 100 mTorr



Surface recombination

- The wall recombination probability, γ_{rec} , is a very important quantity in all low pressure molecular discharges
- We use the wall recombination coefficient measured by Stafford et al. (2009) for stainless steel
- The wall recombination coefficient depends on the dissociation fraction and the wall material



A fit to the measured data is for anodized aluminum

$$\log_{10}(\gamma_{\text{rec}}) = -0.82 - 1.59 \exp\left(-1.81 \times \frac{[\text{Cl}]}{[\text{Cl}_2]}\right)$$

and for stainless steel

$$\log_{10}(\gamma_{\text{rec}}) = -1.22 - 1.34 \exp\left(-1.48 \times \frac{[\text{Cl}]}{[\text{Cl}_2]}\right)$$

Guha et al. (2008) J. Appl. Phys. **103** 013306

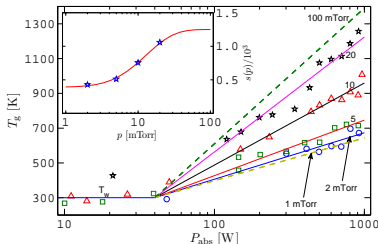
Stafford et al. (2009) J. Phys. D: Appl. Phys. **42** 055206



Gas temperature

- Donnelly and Malyshev (2000) found that the neutral chlorine gas temperature was between 300 and 1250 K, increasing with power and pressure up to 1000 W and 20 mTorr

Donnelly and Malyshev (2000) Appl. Phys. Lett. **77** 2467



A fit through the measured data gives

$$T_g(P_{\text{abs}}, p) = 300 + s(p) \frac{\log_{10}(P_{\text{abs}}/40)}{\log_{10}(40)}$$

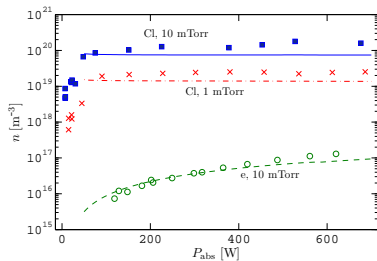
where

$$s(p) = 1250 (1 - e^{-0.091 \times p}) + 400 e^{-0.337 \times p}$$



Comparison with experiments

- Densities of neutral Cl atoms and electrons versus power
- The agreement with the measured electron density is excellent
- The calculated density of atomic chlorine is in a very good agreement with the measured data at both 1 and 10 mTorr



- inductively coupled cylindrical stainless steel chamber
- $L = 20$ cm and $R = 18.5$ cm

Thorsteinsson and Gudmundsson (2010a)

Plasma Sources Sci. Technol. **19** 015001

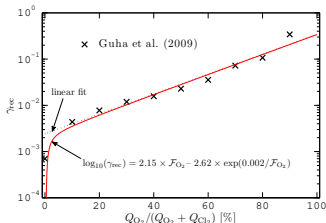
Malyshev and Donnelly (2000) J. Appl. Phys. **88** 6207

Malyshev and Donnelly (2001) J. Appl. Phys. **90** 1130



Dilution with oxygen

- When the chlorine discharge is diluted by oxygen chlorine-oxide molecules, such as ClO or ClO₂ are formed at surfaces
- The desorbing flux of ClO₂ was found to be significantly smaller than that of ClO molecules
- The wall recombination coefficient for ClO production was determined by subtracting the Cl₂ production from the total Cl wall recombination coefficient



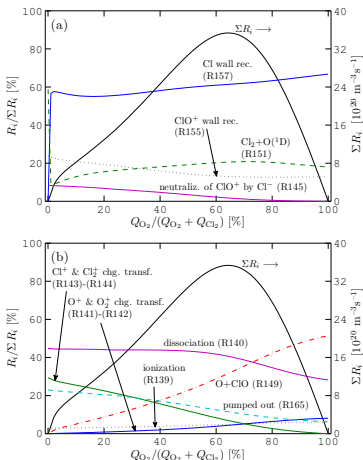
Thorsteinsson and Gudmundsson (2010b)

Plasma Sources Sci. Technol. **19** 055008



Particle densities

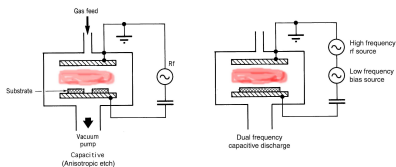
- The total rate for creation and loss of ClO molecules is at maximum when the oxygen content is 65%
- Wall recombination of Cl molecules, is the dominating pathway for creation of ClO molecules
- The bulk processes and recombination of ClO⁺ ions at the wall account for roughly 33–43% of the total rate for ClO creation, combined



2. Surface quenching of metastable molecules



Capacitively Coupled Oxygen Discharge



Lieberman and Lichtenberg (2005) *Principles of Plasma Discharges and Materials Processing*, John Wiley & Sons

- A 1D particle-in-cell/Monte Carlo collision simulation
 - Oxygen discharge
 - Capacitively Coupled Oxygen Discharge at 13.56 MHz
 - surface quenching of $O_2(a^1\Delta_g)$
 - the effect of $\gamma_{see}(\mathcal{E})$
- We use the `oopd1` (objective oriented plasma device for one dimension) code to simulate the discharge
- The discharge model includes energy dependent secondary electron emission yield

Oxygen CCP – pressure dependence

- We apply a voltage source with a single frequency

$$V(t) = V_{\text{rf}} \sin(2\pi ft)$$

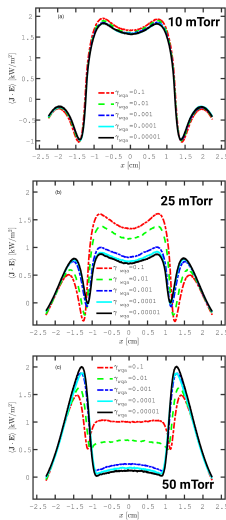
- The electrodes are circular with a diameter of 14.36 cm
- The gap between the electrodes is 4.5 cm
- We set $V_{\text{rf}} = 222$ V and $f = 13.56$ MHz
- The neutrals (O_2 and O) are treated as background gas at $T_{\text{g}} = 300$ K with a Maxwellian distribution
- The dissociation fraction and the metastable fraction is found using a global model
- The pressure is varied from 10 – 50 mTorr



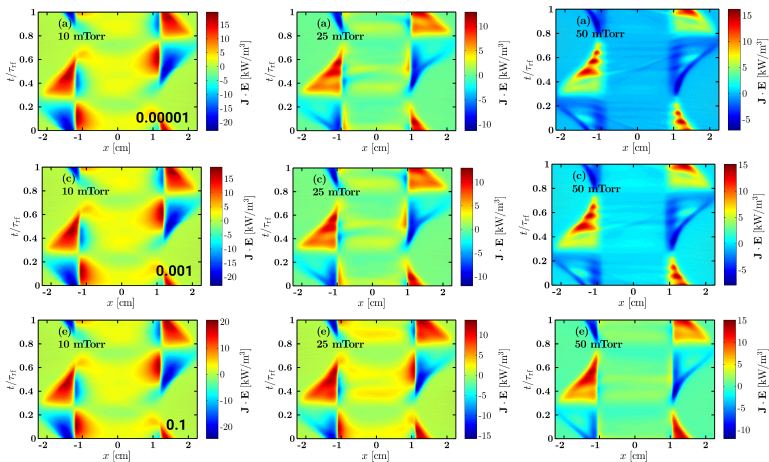
Oxygen CCP – surface quenching of $O_2(a^1\Delta_g)$

- At 10 mTorr almost all the electron heating occurs in the plasma bulk (the electronegative core) and the electron heating profile is independent of the surface quenching coefficient
- At 50 mTorr only for the highest surface quenching coefficients 0.1 and 0.01 there is some electron heating observed in the bulk region
- Typical value is 0.007 for iron (Sharpless and Slinger, 1989)

Proto and Gudmundsson (2018b) PSST 27 074002

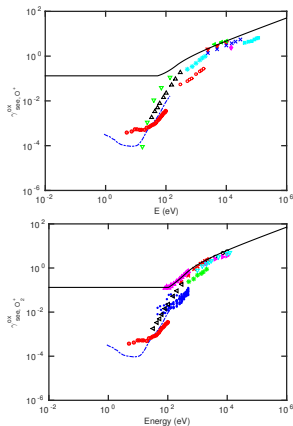


Oxygen CCP – surface quenching of $O_2(a^1\Delta_g)$



The oxygen discharge

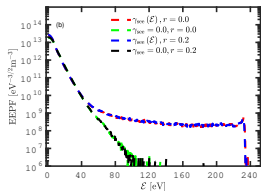
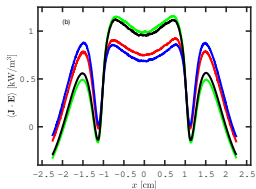
- The discharge model also includes energy dependent secondary electron emission yield
- We have compiled experimental data from the literature on secondary electron emission yields for the species O_2^+ , O^+ , O_2 and O bombarding various metals and substances
- A fit was made through the available experimental data



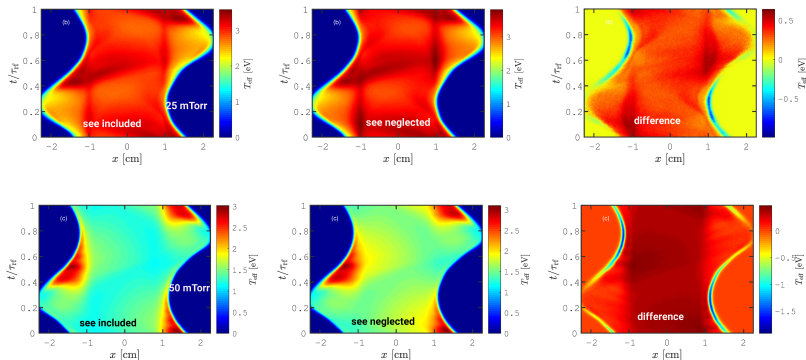
Oxygen CCP – the effect of $\gamma_{\text{see}}(E)$

- Adding secondary electron emission yield
 - increases the electron density
 - increases the electron heating rate in the sheath region
 - the sheath region becomes narrower
 - a high energy tail appears in the EEPF

Hannesdottir and Gudmundsson PSST **25** 055002 (2016)



Oxygen CCP – the effect of $\gamma_{\text{see}}(E)$



Proto and Gudmundsson (2018a) *Atoms* **6**(4) 65

- Including secondary electron emission increases the electron energy and decreases the electron power absorption

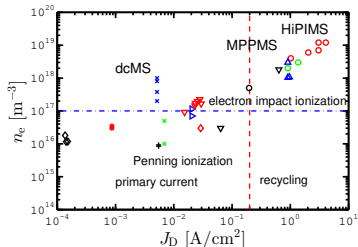
3. Sputter yield

Reactive high power impulse magnetron sputtering (HiPIMS)



Magnetron sputtering discharges

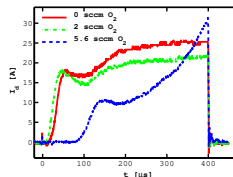
- Magnetron sputtering discharges are widely used in thin film deposition
- In a dcMS the power density (plasma density) is limited by the thermal load on the target
- High ionization of sputtered material requires very high density plasma
- In a HiPIMS discharge a high power pulse is supplied for a short period
 - low frequency
 - low duty cycle
 - low average power



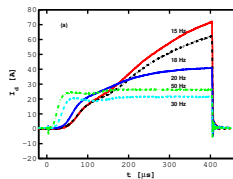
From Gudmundsson (2020) PSST **29** in press

HiPIMS - Voltage - Current - time

- During **reactive sputtering**, a reactive gas is added to the inert working gas and a transition to oxide mode is observed
- The Ar/O₂ discharge with titanium target
- The current waveform is highly dependent on the repetition frequency and applied voltage which is linked to oxide formation on the target
- The current is found to increase significantly as the frequency is lowered



Gudmundsson (2016) PPCF **58** 014002

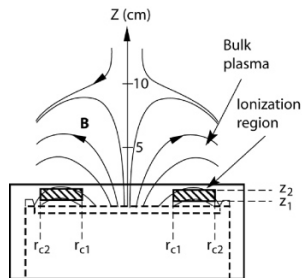


Magnus et al. (2012) JVSTA **30** 050601



Ionization region model studies of reactive HiPIMS

- The ionization region model (IRM) was developed to improve the understanding of the plasma behaviour during a HiPIMS pulse and the afterglow
- It is a time dependent global model of the plasma chemistry of the ionization region (IR) is defined next to the race track
- The IR is defined as an annular cylinder with outer radii r_{c2} , inner radii r_{c1} and length $L = z_2 - z_1$, extends from z_1 to z_2 axially away from the target



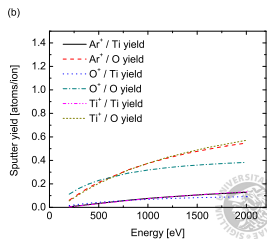
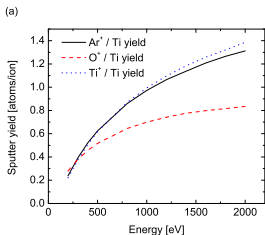
The definition of the volume covered by the IRM

From Raadu et al. (2011) PSST **20** 065007

Ionization region model studies of reactive HiPIMS

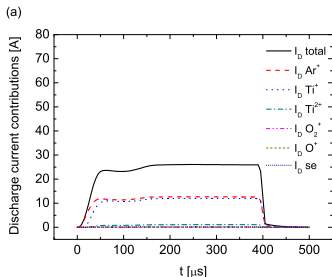
- The sputter yield for the various bombarding ions was calculated by TRIDYN for
 - **Metal mode** – Ti target
 - **Poisoned mode** – TiO₂ target
- The yields correspond to the extreme cases of either clean Ti surface and a surface completely oxidized (TiO₂ surface)
- The sputter yield is much lower for poisoned target

The sputter yield data is from Tomáš Kubart, Uppsala University



Ionization region model studies of reactive HiPIMS

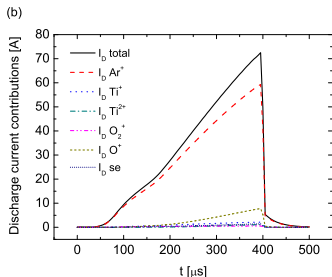
- Ar^+ and Ti^+ -ions contribute most significantly to the discharge current at the cathode target surface – almost equal contribution



The temporal evolution of the neutral species with 5 % oxygen partial flow rate for Ar/O_2 discharge with Ti target in **metal mode**.

Ionization region model studies of reactive HiPIMS

- Ar^+ contribute most significantly to the discharge current – almost solely – at the cathode target surface
- The contribution of secondary electron emission is very small



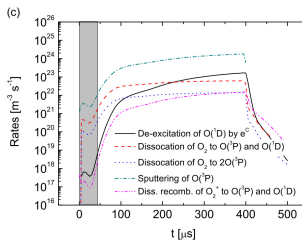
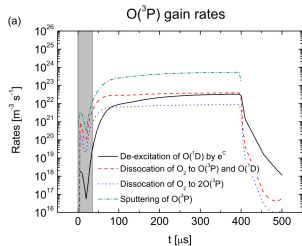
The temporal evolution of the neutral species with 5 % oxygen partial flow rate for Ar/ O_2 discharge with Ti target in **poisoned mode**.

Ionization region model studies of reactive HiPIMS

- The increase in the atomic oxygen in the ground state is due to:
 - sputtering of $O(^3P)$ from the partially to fully oxidized target (dominates)
 - electron impact de-excitation of $O(^1D)$
 - electron impact dissociation of the O_2 ground state molecule

The temporal evolution of the neutral species with **5 % oxygen partial flow rate** for Ar/ O_2 discharge with Ti target in **transition mode** and **poisoned mode**.

Lundin et al. (2017) JAP 121(17) 171917



Summary



Summary

- The importance of surface processes has been demonstrated by a few examples
 - Surface recombination of atoms dictates the dissociation fraction in inductively coupled discharge
 - Surface quenching of molecular metastables dictates the electronegativity and electron power absorption mechanism in a capacitively coupled oxygen discharge
 - The sutter yield determines the dominating ion in a reactive HiPIMS discharge and therefore the dominating the recycling process
- In discharge modeling it is important to include a carefully selected surface process parameters



Acknowledgements

Thank you for your attention

The slides can be downloaded at

<http://langmuir.raunvis.hi.is/~tumi/ranns.html>



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