

# Ionization Processes in the High Power Impulse Magnetron Sputtering Discharge (HiPIMS)

Jón Tómas Guðmundsson

Science Institute, University of Iceland, Iceland

Department of Electrical and Computer Engineering, University of Iceland, Iceland

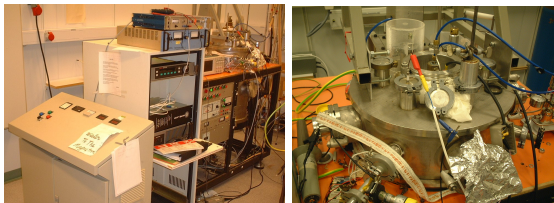
tumi@hi.is

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## Introduction

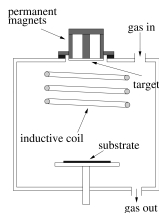
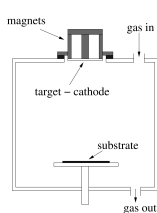
- The demand for new materials and layer structures has lead to development of more advanced sputtering systems
- One such sputtering system is the
  - high power pulsed magnetron sputtering discharge (HPPMS)
  - high power impulse magnetron sputtering discharge (HiPIMS)
- It gives high electron density and highly ionized flux of the sputtered material
- The energy of the ions can be tailored to obtain impinging particles with energies comparable to typical surface and molecular binding energies

## Introduction



- This work is a result of collaboration with
  - Kristinn B. Gylfason (now at Royal Institute of Technology in Stockholm)
  - Dr. Jones Alami (now at RWTH Aachen, Germany)
  - Dr. Johan Bohlmark (now at Chemfikt Ionsputtering AB)
  - Dr. Arutiun Ehiasarian (Sheffield Hallam University, UK)
  - Prof. Ulf Helmersson (Linköping University, Sweden)

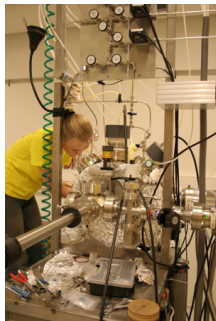
## Planar Magnetron Sputtering Discharge



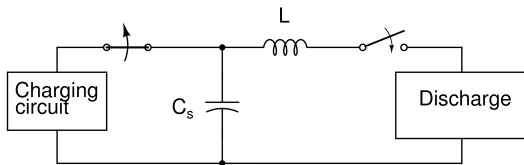
- A typical dc planar magnetron discharge operates at a pressure of 1 – 10 mTorr with a magnetic field strength of 0.01 – 0.05 T and at cathode potentials 300 – 700 V
- Electron density in the substrate vicinity is in the range  $10^{15} - 10^{16} \text{ m}^{-3}$ 
  - low fraction of the sputtered material is ionized ( $\sim 1\%$ )
  - the majority of ions are the ions of the inert gas
  - additional ionization by a secondary discharge (rf or microwave)

## High Power Impulse Magnetron Sputtering (HiPIMS)

- In a conventional dc magnetron discharge the power density is limited by the thermal load on the target
- Most of the ion bombarding energy is transformed into heat at the target
- In unipolar pulsing the power supply is at low (or zero) power and then a high power pulse is supplied for a short period
- The high power pulsed magnetron sputtering discharge uses the same sputtering apparatus except the power supply

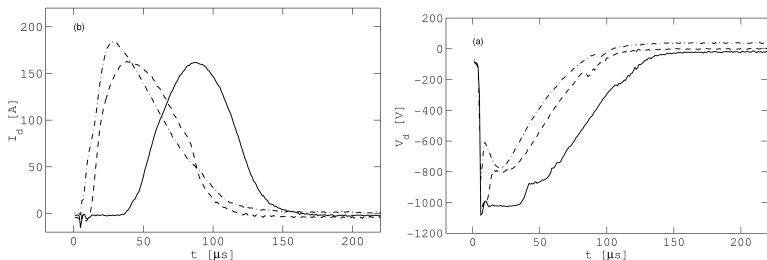


## HiPIMS - Power supply



- The high power pulsed discharge operates with a
  - Cathode voltage in the range of 500-2000 V
  - Current densities of 3-4 A/cm<sup>2</sup>
  - Power densities in the range of 1-3 kW/cm<sup>2</sup>
  - Frequency in the range of 50 – 500 Hz
  - Duty cycle in the range of 0.5 – 5 %

## HiPIMS - Power supply

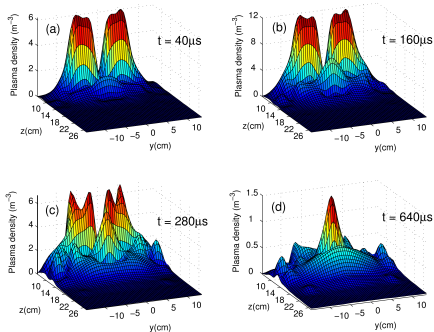


0.5 mTorr (solid line), 2 mTorr (dashed line) and 20 mTorr (dot dashed line)

(After Gudmundsson et al. (2002))

- The exact pulse shape is determined by the load
  - the discharge formed
  - it depends on the gas type and gas pressure

## HiPIMS - Electron density

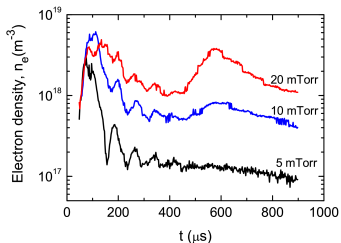


(After Bohlmark et al. (2005b))

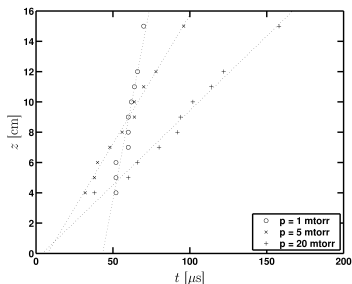
- Temporal and spatial variation of the electron density
- Argon discharge at 20 mTorr with a titanium target
- The electron density in the substrate vicinity is of the order of  $10^{18} \text{ m}^{-3}$



## HiPIMS - Electron density



(After Gudmundsson et al. (2002))

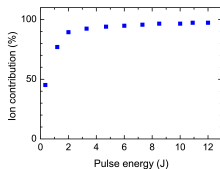


(From Gylfason et al. (2005))

- The electron density versus time from the initiation of the pulse 9 cm below the target
- The pulse is 100  $\mu\text{s}$  long and the average power 300 W
- Each peak travels with a fixed velocity through the chamber

## HiPIMS - Ionization fraction

- There have been conflicting reports on the ionized flux fraction
  - 70 % for Cu (Kouznetsov et al., 1999)
  - 40 % for  $Ti_{0.5}Al_{0.5}$  (Macák et al., 2000)
  - 9.5 % for Al (DeKoven et al., 2003)
  - 4.5 % for C (DeKoven et al., 2003)
- The degree of ionization
  - 90 % for Ti (Bohlmarm et al., 2005a)



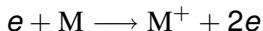
(From Bohlmarm et al. (2005a))

## HiPIMS - Ionization fraction

- To explore the ionization mechanism and the temporal behavior of the plasma parameters a time dependent global (volume averaged) model was developed
- The discharge is assumed to consist of
  - electrons, e
  - argon atoms in the ground state, Ar
  - metastable argon atoms, Ar\*
  - argon ions, Ar<sup>+</sup>
  - metal atoms, M
  - metal ions, M<sup>+</sup>

## HiPIMS - Ionization fraction

- Metal ions are generated by electron impact ionization



by Penning ionization by collision with an electronically excited argon atom



by charge exchange



- The metal ions are assumed to be lost by diffusion to solid surfaces such as the chamber walls

## HiPIMS - Ionization fraction

- Particle balance for metal ions

$$\frac{dn_{m+}}{dt} = \underbrace{k_{\text{miz}} n_e n_m}_{\text{electron impact}} + \underbrace{k_P n_{\text{Ar}^*} n_m}_{\text{Penning}} + \underbrace{k_{\text{chexc}} n_{\text{Ar}^+} n_m}_{\text{charge exchange}} - \underbrace{k_{\text{wall},m+} n_{m+}}_{\text{loss to wall}}$$

- Particle balance for metal atoms

$$\begin{aligned} \frac{dn_m}{dt} = & \underbrace{\frac{\gamma_{\text{sput}} h_L u_B n_{\text{Ar}^+} r_T^2}{R^2 L}}_{\text{sputtering from target}} + \underbrace{\frac{\gamma_{\text{selfsput}} h_L u_{B,m} n_{m+} r_T^2}{R^2 L}}_{\text{selfsputtering from target}} \\ & - \underbrace{k_{\text{miz}} n_e n_m}_{\text{ionization}} - \underbrace{k_P n_{\text{Ar}^*} n_m}_{\text{Penning}} - \underbrace{k_{\text{chexc}} n_{\text{Ar}^+} n_m}_{\text{charge exchange}} - \underbrace{k_{\text{diff},m} n_m}_{\text{loss to wall}} \end{aligned}$$

## HiPIMS - Ionization fraction

- Particle balance for argon ions,  $\text{Ar}^+$

$$\frac{dn_{\text{Ar}^+}}{dt} = k_{\text{iz}} n_e n_{\text{Ar}} + k_{\text{exc,iz}} n_e n_{\text{Ar}^*} - k_{\text{chexc}} n_m n_{\text{Ar}^+} - k_{\text{wall,Ar}^+} n_{\text{Ar}^+}$$

- Particle balance for metastable argon atoms,  $\text{Ar}^*$

$$\frac{dn_{\text{Ar}^*}}{dt} = k_{\text{exc}} n_e n_{\text{Ar}} - (k_{\text{exc,iz}} + k_{\text{deexc}}) n_e n_{\text{Ar}^*} - k_{\text{loss,Ar}^*} n_{\text{Ar}^*} - k_{\text{p}} n_{\text{Ar}^*} n_m$$

- Quasi-neutrality condition

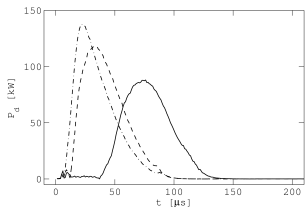
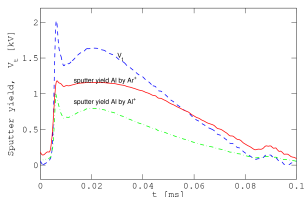
$$n_e = n_{\text{Ar}^+} + n_{\text{m}^+}$$

- Power balance

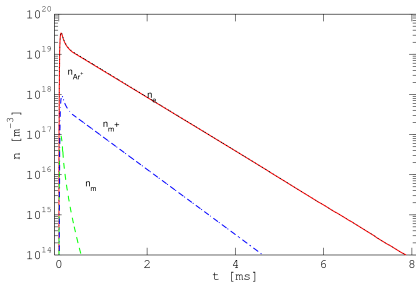
$$\frac{d}{dt} \left( \frac{3}{2} e n_e T_e \right) = \frac{P_{\text{abs}}}{V} - e \mathcal{E}_c k_{\text{iz}} n_{\text{Ar}} n_e - e k_{\text{wall,Ar}^+} (\mathcal{E}_e + \mathcal{E}_i) n_{\text{Ar}^+}$$

## HiPIMS - Ionization fraction

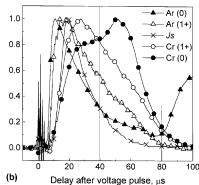
- The temporal variation of the particle density and the electron temperature was obtained by solving the differential equations simultaneously and self-consistently
- We assume a discharge chamber of radius  $R = 15$  cm and length  $L = 15$  cm with a target of radius 7.5 cm made of aluminum.
- The electron energy distribution is assumed to be Maxwellian
- The power pulse is the measured pulse at 10 mTorr (dash dot line)



## HiPIMS - Ionization fraction



- The calculated electron and ion density versus time

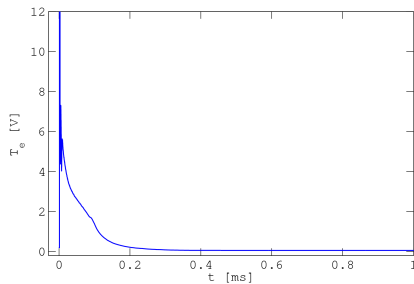


From Ehiasarian et al. (2002)

- The measured emission from a discharge with a Cr target



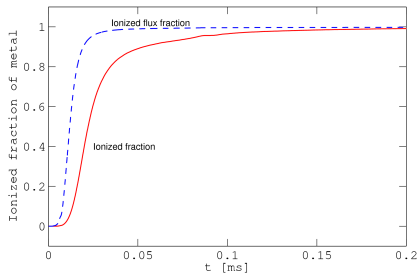
## HiPIMS - Ionization fraction



- The calculated electron temperature

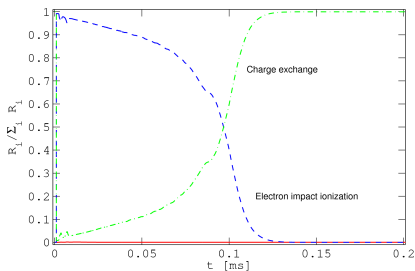
## HiPIMS - Ionization fraction

- For aluminum
  - The integrated ionized fraction is 97 %
  - The integrated ionized flux fraction is 99 %
- For carbon
  - The integrated ionized fraction is 89 %
  - The integrated ionized flux fraction is 97 %



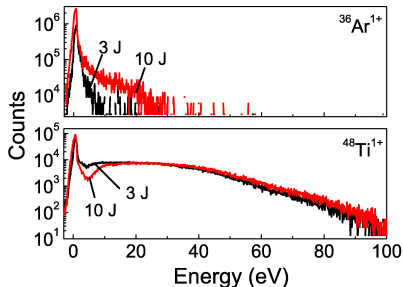
## HiPIMS - Ionization fraction

- The first 100  $\mu\text{s}$  (while the pulse is “on”) electron impact ionization is the most effective process in creating metal ions
- Then charge exchange becomes the dominant process in creating metal ions



## HiPIMS - Ion energy

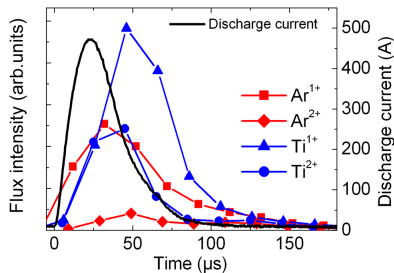
- The time averaged ion energy distribution for  $\text{Ar}^+$  and  $\text{Ti}^+$  ions
- The gas pressure was 3 mTorr, pulse energy 3 J and 10 J and the target made of Ti
- The ion energy distribution is broad to over 100 eV
- About 50 % of the  $\text{Ti}^+$  ions have energy  $> 20$  eV



(From Bohlmark et al. (2006))

## HiPIMS - Ionization fraction

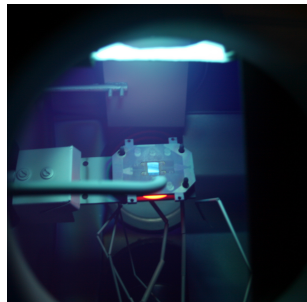
- The ion flux versus time measured by a mass spectrometer ( $20 \mu\text{s}$  windows)
- The gas pressure was 3 mTorr, pulse energy 8 J and the target made of Ti



(From Bohlmark et al. (2006))

## HiPIMS - Deposition rate

- Several groups report on a significantly lower deposition rate for HiPIMS as compared to dcMS
  - a factor of 2 lower deposition rate for Cu and Ti thin films (Bugaev et al., 1996)
  - a factor of 4 – 7 lower deposition rate for reactive sputtering of  $\text{TiO}_2$  from a Ti target (Davis et al., 2004)
  - a factor of 3 - 4 lower deposition rate for reactive sputtering of  $\text{AlO}_x$  from an Al target (Sproul et al., 2004)
  - the reduction in deposition rate decreases with decreased magnetic confinement (weaker magnetic field) (Bugaev et al., 1996)



## HiPIMS - Deposition rate

- One explanation is that the sputtered material is ionized close to the target and many of the metallic ions will be attracted back to the target surface by the cathode potential
- A reduction in the deposition rate would occur mainly for metals with a low self-sputtering yield
- Maybe this can be reduced by optimized magnetic confinement

## Summary

- We reviewed the physics of the high power impulse magnetron sputtering discharge (HIPIMS)
- Power supply
  - Essentially the same sputtering apparatus except for the power supply
- Electron density
  - Roughly 2 orders of magnitude higher in the substrate vicinity than for a conventional dc magnetron sputtering discharge
- Plasma dynamics
  - The peak electron density travels away from the target with fixed velocity



## Summary

- Ionization fraction
  - Ionization fraction is high, mainly due to the high electron density
  - The ions on the inert gas and the ions of the sputtered vapor are separated in time
- Deposition rate
  - Deposition rate is lower than in a conventional dc magnetron sputtering discharge, maybe due to self sputtering

## References

- Bohlmarm, J., Alami, J., Christou, C., Ehiasarian, A. P., and Helmersson, U. (2005a). Ionization of sputtered metals in high power pulsed magnetron sputtering. *Journal of Vacuum Science and Technology A*, 23(1):18–22.
- Bohlmarm, J., Gudmundsson, J. T., Alami, J., Latteman, M., and Helmersson, U. (2005b). Spatial electron density distribution in a high-power pulsed magnetron discharge. *IEEE Transactions on Plasma Science*, 33(2):346–347.
- Bohlmarm, J., Latteman, M., Gudmundsson, J. T., Ehiasarian, A. P., Gonzalvo, Y. A., Brenning, N., and Helmersson, U. (accepted for publication 2006). The ion energy distribution and ion flux composition from a high power impulse magnetron sputtering discharge. *Thin Solid Films*.
- Bugaev, S. P., Koval, N. N., Sochugov, N. S., and Zakharov, A. N. (1996). Investigation of a high-current pulsed magnetron discharge initiated in the low-pressure diffuse arc plasma. In *XVIIIth International Symposium on Discharges and Electrical Insulation in Vacuum, 1996*, pages 1074–1076, Berkeley, CA USA. IEEE.
- Davis, J. A., Sproul, W. D., Christie, D. J., and Geisler, M. (2004). High power pulse reactive sputtering of  $\text{TiO}_2$ . In *47th Annual Technical Conference Proceedings*, pages 215–218, Dallas, TX, USA. Society of Vacuum Coaters.
- DeKoven, B. M., Ward, P. R., Weiss, R. E., Christie, D. J., Scholl, R. A., Sproul, W. D., Tomasel, F., and Anders, A. (2003). Carbon thin film deposition using high power pulsed magnetron sputtering. In *46th Annual Technical Conference Proceedings*, pages 158–165, San Francisco, CA, USA. Society of Vacuum Coaters.
- Ehiasarian, A. P., New, R., Münz, W.-D., Hultman, L., Helmersson, U., and Kouznetsov, V. (2002). Influence of high power densities on the composition of pulsed magnetron plasmas. *Vacuum*, 65:147–154.
- Gudmundsson, J. T., Alami, J., and Helmersson, U. (2002). Spatial and temporal behavior of the plasma parameters in a pulsed magnetron discharge. *Surface and Coatings Technology*, 161(2-3):249–256.
- Gylfason, K. B., Alami, J., Helmersson, U., and Gudmundsson, J. T. (2005). Ion-acoustic solitary waves in a pulsed magnetron sputtering discharge. *Journal of Physics D: Applied Physics*, 38(18):3417–3421.

- Helmersson, U., Lattemann, M., Alami, J., Bohlmark, J., Ehiasarian, A. P., and Gudmundsson, J. T. (2005a). High power impulse magnetron sputtering discharges and thin film growth: A brief review. In *48th Annual Technical Conference Proceedings*, pages 458 – 464, Denver, CO, USA. Society of Vacuum Coaters.
- Helmersson, U., Lattemann, M., Bohlmark, J., Ehiasarian, A. P., and Gudmundsson, J. T. (2005b). Ionized physical vapor deposition (IPVD): A review of technology and applications. *Thin Solid Films* 515(1):1–24.
- Kouznetsov, V., Macák, K., Schneider, J. M., Helmersson, U., and Petrov, I. (1999). A novel pulsed magnetron sputter technique utilizing very high target power densities. *Surface and Coatings Technology*, 122(2-3):290–293.
- Macák, K., Kouznetsov, V., Schneider, J. M., Helmersson, U., and Petrov, I. (2000). Ionized sputter deposition using an extremely high plasma density pulsed magnetron discharge. *Journal of Vacuum Science and Technology A*, 18(4):1533–1537.
- Sproul, W. D., Christie, D. J., Carter, D. C., Tomasel, F., and Linz, T. (2004). Pulsed plasmas for sputtering applications. *Surface Engineering*, 20:174–176.